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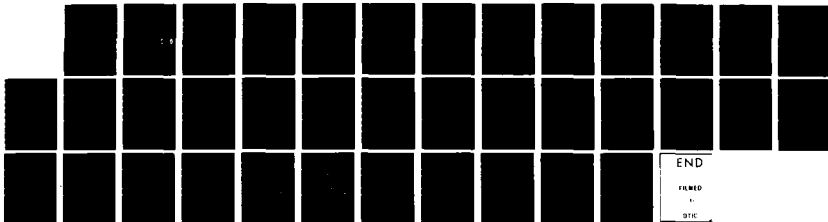
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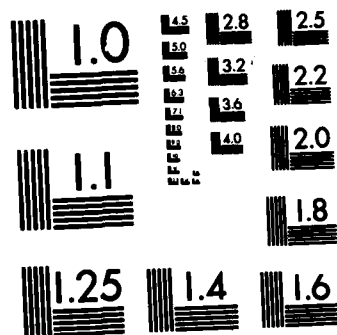
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Phase Equilibria and Transition in Mixtures
of a Homopolymer and a Block Copolymer
II. The Phase Diagram

by

R. J. Roe and W. C. Zin

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ABSTRACT

The phase relationship in mixtures containing a block copolymer and a homopolymer has been studied by means of light scattering. The copolymer employed is a styrene-butadiene block copolymer of molecular weight (M_w) 28000, containing 27% styrene. The homopolymer in the mixture is either 1) polystyrene of M_w 2400, 2) polystyrene of M_w 3500, or 3) polybutadiene of M_w 26000. The first system containing the lower molecular weight polystyrene was previously studied in detail also by means of small-angle X-ray scattering. The observed cloud points show a change with temperature in the limit of solubility of the homopolymers in the block copolymer, which has an ordered, microdomain structure at low temperatures but a disordered, homogeneous structure at high temperatures. The observed solubility limits at low temperatures turn out to be greater, by an order of magnitude, than the prediction based on an earlier block copolymer theory. The phase diagram, constructed on the basis of the light and X-ray scattering data, is rich in features and resembles the complex phase diagrams often observed with binary metal alloys. The possibility of observing a critical phenomenon, at a certain ratio of the homopolymer chain length to the block chain length, is pointed out.

I. INTRODUCTION

When a small amount of a homopolymer A is added to a block copolymer A-B possessing ordered microdomain structure, the homopolymer is readily accommodated in the microdomains consisting of A blocks of the copolymer. As more of the homopolymer is added, a solubility limit is eventually reached, and a phase consisting mainly of the homopolymer separates out. The solubility limit is governed by the relative lengths of the homopolymer A and the block A in the copolymer as well as by the microdomain structure of the latter.

When a change in the microdomain structure is induced by heating such a mixture, the solubility limit is altered accordingly. A pronounced change in the thermodynamic behavior of the mixture can occur in particular when the block copolymer structure undergoes a transition, on heating, to a homogeneous, disordered structure. Such a transition can be observed, in the experimentally accessible temperature range, if the block lengths are relatively short or the two blocks of the copolymer are only moderately incompatible.

Part I¹ of the present series of papers reported the result of a small-angle X-ray scattering study on a system of mixtures of a low molecular weight polystyrene with a styrene-butadiene block copolymer, and described the change in their structure observed as a function of polystyrene concentration and temperature. The present article reports the result of light scattering study on the same system and also on two other related systems of mixtures. The observed cloud point reveals

the onset of separation into phases which are much larger than the microphases detected by the small-angle X-ray technique. The three systems investigated are as follows. One of the components of all the mixtures is a styrene-butadiene diblock copolymer containing about 25% styrene. The second component is a homopolymer which is either a polystyrene of M_w 2400, a polystyrene of M_w 3500, or a polybutadiene of M_w 26000.

The microdomains are of sizes much smaller than the wavelength of light, and therefore the mixtures having a microdomain structure at low temperatures remain transparent to light as long as the amount of the homopolymer is within the solubility limit. When the mixture is heated and the microdomain structure is disrupted, the resulting disordered block copolymer is often no longer compatible with the homopolymer, unless the temperature is very high. Thus, when such a mixture is heated from room temperature, it is at first clear, but becomes suddenly turbid at a certain temperature and remains so until, at an even higher temperature, it becomes clear again. The temperatures of transition from clear to turbid and then back to clear states of course depend on the concentration of the homopolymer. The observed cloud point curves, obtained as a function of the temperature and the composition, and the phase diagram deduced from them exhibit interesting complexities resembling those obtained frequently with binary metal alloys.

The solubility limits of homopolymers in the block copolymer microdomains are found to decrease as the ratio of the homopolymer chain length to the corresponding block sequence

length is increased. This is in accord with the expectation based on one of the early block copolymer theories. Quantitatively, however, the observed solubility limits turn out to be greater than the prediction by an order of magnitude.

With the temperature, the concentration, and the molecular weights of the components as the variables at our disposal, the mixtures containing block copolymers can be made to exhibit a wealth of features of theoretical and practical interest. The light scattering and small-angle X-ray scattering techniques are complementary to each other for the study of these systems, as they provide structural information on different size scales.

II. EXPERIMENTAL SECTION

Material

The styrene-butadiene diblock copolymer contains 27% (by weight) of styrene, as determined by NMR, and its M_w and M_n (determined by GPC) are 28000 and 27000 respectively. This is the same material studied in our previous work¹⁻³. Characterization data of this polymer has also been reported by Krause et al.⁴ The polybutadiene has M_w and M_n (determined by GPC) equal to 26000 and 25000 respectively. The diblock copolymer and the polybutadiene were kindly synthesized for us by Dr. H. L. Hsieh of Philips Petroleum Co. The two polystyrenes used were of M_w 2400 and 3500 and were obtained from Pressure Chemical Co. These three homopolymers were also used in our previous work² and more detailed characterization data were given there.

Method

Construction of the light scattering apparatus and the method of measurements were described in the previous publication.² In particular, the polymer mixtures were prepared, without solvent, in a glass tube which was subsequently sealed under vacuum. A magnetically activated glass stirrer, also sealed in the tube, was used to mix the components at high temperatures at which they are compatible. A low-power He-Ne laser was used as the light source and the intensity of light scattered at a 90° angle was measured with a photodiode.

After a preliminary determination of the approximate cloud point, the temperature of the sample was cycled up and down over a 40-60 degree interval around the cloud point by means of a temperature programmer, and the outputs of the thermocouple and the light detector were continuously recorded on a chart recorder. A heating/cooling rate of 1°/min was used ordinarily, except at temperatures above 180°C where a 2°/min rate was used to minimize the possibility of thermal degradation. The effect of different heating rates is illustrated in Fig. 1, where the intensity (or the output of the photodiode in mV) of light scattered from a mixture containing the block copolymer and 25% of 2400 molecular weight polystyrene is plotted against temperature. The three curves were obtained at 4°/min, 2°/min, and 0.5°/min, and only a minor difference is noted between the last two cases. A downward extrapolation of the steep linear increase beyond 150°C intersects with the base-line at about

156°C, which is taken as the cloud point. The element of subjective judgement in the extrapolation procedure appears to introduce an uncertainty of not more than 4° in the cloud point thus determined. The reproducibility on duplicate runs is within 2°. The cloud points determined on heating and cooling are usually found to differ by a few degrees. Those determined on a temperature change in the direction of decreasing turbidity are reported in this paper.

III. RESULTS

The cloud point curves obtained with the three mixture systems are given in Figs. 2-4. The system containing the block copolymer and the polystyrene (M_w 2400) was studied in more detail than the other two. This system was also examined by small-angle X-ray scattering as reported in Part I.

In region I, in Fig. 2, the mixture is visually transparent although there is a tendency for the scattered intensity to increase slightly with increasing temperature as seen in Fig. 1. In crossing from region I to IV, the turbidity increases very steeply, and the mixture becomes opaque, giving all the appearance of macroscopic phase separation. In region II the mixture is again transparent and behaves as a homogeneous liquid of moderate viscosity. In region III the mixture remains moderately cloudy throughout, with its turbidity tending to increase somewhat as the temperature is lowered toward room temperature. Region III is considered to arise as a result of the mixture separating into two phases, the one consisting of

the block copolymer swollen with the polystyrene but still maintaining the microdomain structure, and the other of the polystyrene with suspended block copolymer micelles. The boundary between regions I and III, in Fig. 2, is slightly inclined from the temperature axis. Thus, when a mixture containing 48% of the polystyrene, which is in region III at room temperature, is heated, it becomes clear on crossing into region I at 90°C, and then sharply cloudy again on crossing into region IV at 110°C. The opaqueness in region IV is much greater than in region III. As a result, on heating a mixture containing, for example, 60% polystyrene, the scattered intensity sharply increases as it crosses from region III to region IV at around 120°C. This suggests, therefore, that although both regions III and IV represent conditions for coexistence of macroscopic phases, the nature of the phases which separate out are different. In both cases, one of the phases is the ordered block copolymer swollen with polystyrene. The second phase which coexists with it in region III and in region IV will be discussed in the next section.

To illustrate the degree of sharpness of the transitions between different regions, the scattered intensities observed at 80° and 140°C are replotted as a function of the composition of the mixture in Fig. 5. The arrows denote the cloud points determined from the original chart recordings of the intensity against temperature. At 80°C the cloudy mixture is in region III and at 140°C it is in region IV, and the difference between these two regions is illustrated by the widely different levels

of scattered intensity.

The features observed with the other two systems, shown in Figs. 3 and 4, are generally similar to those described above, but some minor differences are to be noted. With these two systems, the boundary between regions I and III is parallel with the temperature axis within the experimental uncertainty. Also, the turbidity in region III is generally much higher than is observed with the first system, and as a result it is difficult to determine the boundary between regions III and IV except when the concentration of the homopolymer is only moderately in excess of the solubility limit, as seen in Figs. 3 and 4.

IV. DISCUSSIONS

The experimentally obtained solubility limits of the three homopolymers in the styrene-butadiene block copolymer at low temperatures are given in Table I. The solubility limits are expressed in four different ways. Row 4 gives the weight fraction of the homopolymer in the mixture, as read off directly from Figs. 2, 3, and 4. Row 5 gives the weight fraction of monomers A belonging both to the homopolymer and the block A of the copolymer. Row 6 gives the volume fraction, p , of the homopolymer in the microdomains in which it is dissolved. Row 7 gives the ratio, q , of the volume of dissolved homopolymer to the volume of the solubilizing block; $q = p/(1-p)$. The solubility is seen to decrease as the relative size of the dissolving homopolymer becomes larger and the molecular weight

ratio, M_H/M_A , of the homopolymer to the solubilizing block of the copolymer increases.

The only theory available for comparison with our solubility data is the one due to Meier.⁵ The values calculated from his theory for the case of diblock copolymers having equal lengths of A and B blocks and forming a lamellar microdomain structure are given in row 8 of Table I. The trend of change in the solubility as a function of the molecular weight ratio is correctly predicted, but the theory underestimates the solubility by an order of magnitude. In his theory, five factors affecting the free energy of mixing are considered. They are a) the microdomain interfacial energy, b) the entropy of junction confinement, c) constraints and distortions to the block copolymer chain conformation, d) constraints to the homopolymer conformation, and e) the entropy of mixing. Factor c) accounts for the entropy loss associated with the confinement of copolymer blocks within their respective microdomains and also with the distortion to their conformation out of the necessity of maintaining a constant density throughout the microdomain. Meier defines a chain perturbation parameter α to represent the degree of extension of the block chain end-to-end distance and equates it to the ratio of the thickness of the lamellar microdomain to the unperturbed end-to-end distance of the block chain. As the microdomain becomes swollen with solubilized homopolymers, according to the theory, α becomes larger and therefore the conformational entropy of the block chain is further reduced. It is likely,

however, that α becomes smaller, rather than larger, as more homopolymer is dissolved. The requirement of maintaining a constant density can now be satisfied more easily by placing more of the homopolymer molecules toward the central part of the lamellae which otherwise had to be filled by highly stretched block chains. The conformational entropy of the block chains is thus increased with homopolymer solubilization and provides the additional driving force which probably accounts for the observed solubility much greater than predicted by the original theory.

The data given in Figs. 2, 3, and 4 show that the solubility of the homopolymers at low temperatures is fairly insensitive to the temperature variation. This means that the solubility limits are determined, to a first approximation, solely by an entropy effect. This should be particularly true at temperatures low enough to make the assumption of thin interfaces valid. The solubility limit is then a function of three parameters defining the systems: the molecular weight M_H of the homopolymer and the molecular weights M_A and M_B of the two blocks of the copolymer. (A denotes the block having the same monomer as the homopolymer.) Since changing the three molecular weights by equal factors does not alter the geometry of the system, the solubility limit can actually be given as a function of two variables

$$p = (M_H/M_A, M_B/M_A) \quad (1)$$

In Fig. 6, the values of p in row 6 of Table I are plotted against M_H/M_A . The value of M_B/M_A for the third point (with polybutadiene) is actually different from the same for the first two (with polystyrene), and in making this plot we have in effect neglected the influence of the variable M_B/M_A in eq. (1). The ratio M_B/M_A affects the solubility mostly through its role as a factor in determining the geometry (spherical, cylindrical, or lamellar) of the microdomains attained. Although there is a good reason to believe that the solubility in spherical microdomains will be somewhat less than in lamellae under otherwise identical conditions, the difference is probably small and can be neglected in this semi-quantitative discussion. (According to Leibler's theory⁶, all block copolymers, irrespective of the ratio M_B/M_A , attains a lamellar structure at sufficiently low temperatures, and if that is the case, the variable M_B/M_A in eq. (1) can legitimately be neglected.) The solid line drawn through the points flattens out at low values of M_H/M_A and suggests that the homopolymer will be soluble in the block copolymer at all concentrations when M_H/M_A is below about 0.3.

When a mixture consists mostly of a homopolymer and contains only a small concentration of a block copolymer, the latter is likely to aggregate into micelles and become suspended in the continuous matrix of the homopolymer. With increasing concentration, the block copolymer micelles may eventually aggregate further into ordered arrays of microdomains swollen with the homopolymer. The broken line on the right in Fig. 6

has been drawn from a qualitative consideration to represent the limit of stability of micellar suspension. A mixture with a composition within the range bounded by the solid curve on the left and the broken curve on the right then should separate spontaneously into two phases, each having the composition represented by these two curves. Fig. 6 in fact resembles the phase diagram of a binary liquid mixture if the M_H/M_A axis is replaced by the temperature axis. In Fig. 6 there then should exist a critical point C at which the distinction between the microdomain structure and the micellar solution disappears and, in addition, the mixture exhibits a large fluctuation in the density of micelles (or microdomains). Our data suggest that such a critical point is attained when M_H/M_A is approximately equal to 0.3 and p is between 0.8 and 0.9.

On the basis of the observed cloud point curves and of general thermodynamic principles governing phase relations, phase diagrams are constructed and are shown in Fig. 7 for the mixtures containing the polystyrene ($M_w = 2400$) and in Fig. 8 for those containing the polybutadiene. Some of the observed cloud points are indicated in these figures with circles, and the temperatures of transition from an ordered morphology to a disordered structure, determined¹ by small-angle X-ray scattering, are also indicated by squares. In the two liquid phases, designated L_1 and L_2 , the block copolymer is molecularly dispersed and no aggregated structure of the latter, either in the form of micelles or microdomains, remain. In the meso phase M_1 , the microdomains, swollen with dissolved homopolymer, are

organized into an ordered structure. The micellar phase M_2 , in which micellar aggregates of block copolymers are suspended with no ordering among them, is considered to constitute a separate phase.

Point A in Fig. 7 represents the disordering temperature of the pure block copolymer. At small polystyrene concentrations, the boundary between phases M_1 and L_1 is indicated by two lines AB and AC enclosing a small region in which the two phases coexist. These two lines are drawn here mainly to make it accord with the rules⁷ governing the binary phase diagrams. These rules apply strictly only when the underlying phase transition is of a first order. In block copolymer systems, the transition from an ordered to a disordered state is very diffuse. Our previous study³, by small-angle X-ray scattering, of the same diblock copolymer as used here shows that the intensity of X-ray scattering due to the ordered structure diminishes continuously, without any sudden change, as the temperature is raised. This indicates that the order in the organization of the block copolymer molecules undergoes no discontinuous transition but rather gradual and continuous modifications. When the block copolymer is mixed with small concentrations of homopolymer, the transition is again gradual, as ascertained from our small-angle X-ray study¹. It in a way resembles the phenomenon of the so-called "order-disorder" transition in binary alloys. In such cases, it is known that the transition between an ordered to a disordered phase can occur without an intervening region of two-phase stability. The

transition points in Fig. 7, indicated by squares, were obtained from X-ray measurements while no increase in the optical turbidity was noted in the corresponding temperature range. This shows that in this system the two lines AB and AC in fact coalesce into one.

The line CE in Fig. 7 shows that the solubility of homopolymer in the ordered block copolymer phase decreases rather rapidly with increasing T in this moderately high temperature range. According to Le Chatelier's principle, the equilibrium point of a system shifts with increasing T toward a higher energy state. In our system an increase in the energy can arise only from an increased number of unfavorable contacts between different types of monomers, if we neglect the minor effect due to the change in the polymer conformation with temperature. Since the solubility of homopolymer in the block copolymer is observed to decrease at higher T, the only way of increasing the energy of the system is through increased mixing of the A and B blocks in the copolymer. In our previous study³, in order to explain the gradual, continuous decrease in the X-ray intensity scattered from the pure block copolymer, we proposed that the transition from an ordered to a disordered structure proceeds through gradual intermixing of the component blocks in the microdomains. The negative temperature dependence of the homopolymer solubility, shown by curve CE, supports this view. In fact, the increase in the degree of intermixing of blocks with T is so steep that the dissolved homopolymer is driven out of the block copolymer microdomains and forced to form a separate phase.

In Fig. 7, curves FI and FJ, denoting the limits of stability of the micellar solution phase, are based on a conjecture. In drawing these curves, the following observations are taken into consideration. 1) The two curves, CE and EH, denoting the homopolymer solubility limits in the ordered block copolymer, meet at an angle at E instead of forming a continuous single curve. ii) The turbidity in region IV having coexisting M_1 and L_2 phases is much higher than in region III below the line EG. The discontinuity at E suggests the presence of a triple point, which can be accounted for by the formation of the micellar solution phase M_2 . The lower turbidity below the triple point suggests that the two phases which coexist have a much smaller difference in composition between them (curves EH and FI) in comparison to the two phases which coexist above the triple point (curves CE and DG). The region corresponding to the area GFIK has not been studied carefully in this work and remains the subject of future study. The location of F has yet to be determined. The boundary between regions III and IV in Fig. 2 does not lie on a constant temperature, which is required from the phase rule if it indeed is a triple point, and it is not clear whether this discrepancy arises solely from the difficulty of determining the cloud point between two regions which are both turbid. Another interesting question which has to be settled in the future is whether the micellar solution phase M_2 exists as a phase distinct from the true solution phase L_2 and separated by an intervening two phase region GFJK.

The phase diagram for the mixtures containing

polybutadiene, shown in Fig. 8, is qualitatively similar to Fig. 7, except in one aspect. At low concentration of polybutadiene, the curve giving the temperature of transition from an ordered to a disordered structure has a negative slope here, whereas in the case of the mixtures containing polystyrene it has a positive slope. This probably arises from the asymmetry of the block copolymer sample used here -- 27% styrene against 73% butadiene. Thus, when polystyrene is added, the mixture becomes a little more symmetrical, approaching toward an equal proportion of the two types of monomers, whereas when polybutadiene is added the mixture becomes even more asymmetric. In the theory of block copolymers by Leibler⁶, the transition temperature is predicted to decrease as the relative size of the blocks becomes more disparate (while the total chain length of the copolymer remains the same). A qualitatively similar trend evidently results even when the relative amount of the monomers is altered by addition of homopolymers as in our systems.

The phase equilibria at temperatures above the "pseudo-triple point" BCD can be interpreted in terms of the free energy of mixing of two polymer liquids, if the disordered block copolymer is assumed to behave essentially as the corresponding random copolymer does. The observed cloud points dividing regions II and IV in Figs. 2 and 4 are therefore analyzed by means of the Flory-Huggins expression:

$$\Delta G_M = RT[(1/V_1)\phi_1 \ln \phi_1 + (1/V_2)\phi_2 \ln \phi_2] + \Lambda_{12}\phi_1\phi_2 \quad (2)$$

where ΔG_M is the free energy change, per unit volume, of mixing component 1 of molar volume V_1 and component 2 of molar volume V_2 , and ϕ_1 and ϕ_2 are the volume fractions. Λ_{12} is the polymer-polymer interaction parameter, and is treated here as a parameter to be determined by comparison with the experimental data. Λ_{12} is related to the more usual χ parameter through:

$$\chi = \Lambda V_{\text{ref}} / RT \quad (3)$$

where the reference volume V_{ref} is often taken equal to the monomer volume. Our reason for preferring Λ to χ was given previously². When one (or both) of the components is a random copolymer, the experimentally determined Λ_{12} can be related² to the interaction parameter Λ_{AB} between the homopolymers A and B by

$$\Lambda_{AB} = \Lambda_{12} / (f_{A1} - f_{A2})^2 \quad (4)$$

where f_{A1} and f_{A2} are the fractions of the comonomer A in components 1 and 2 respectively.

Since Λ_{12} usually depends on the temperature and the composition of the mixture moderately, we write:

$$\Lambda_{12} = \lambda_0 + \lambda_T T + \lambda_1 \phi_1 \quad (5)$$

and seek the values of the adjustable parameters λ_0 , λ_T and λ_1 which give a best fit to the observed cloud points. The results

are summarized in Table II. The last column in the table gives the value of Λ_{AB} calculated according to eq. (4) at 200°C and $\phi_1=0.5$. The values obtained in the current work from the mixtures of a block copolymer and a homopolymer agree well with the average of the previous values obtained from the study² of homopolymer mixtures and mixtures of a homopolymer with a random copolymer. The temperature coefficients of Λ_{AB} given in the 6th column in the table, however, are larger than the average of the previous results. This suggests the possibility that a block copolymer, even when disordered, exhibits properties which deviate more from those of the corresponding random copolymer as the temperature is lowered.

ACKNOWLEDGEMENT

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REFERENCES

1. Zin, W.-C.; Roe, R.-J., manuscript in preparation.
2. Roe, R.-J.; Zin, W.-C., *Macromolecules* 1980, 13, 1221.
3. Roe, R.-J.; Fishkis, M.; Chang, J. C., *Macromolecules* 1981, 14, 1091.
4. Krause, S.; Lu, Z.-H., Iskander, M., *Macromolecules* 1982, 15, 1076.
5. Meier, D. J., *Polymer Preprint* 1977, 18(1), 340.
6. Leibler, L., *Macromolecules* 1980, 13, 1602.
7. Gordon, P., 'Principles of Phase Diagrams in Materials Systems', McGraw-Hill Book Co., New York, 1968.

Table I

Solubility of Homopolymer in Block Copolymer

Homopolymer	Polystyrene	Polystyrene	Polybutadiene
1. M_w of homopolymer H, M_H	2,400	3,500	26,000
2. MW of the block A ^a , M_A	7,600	7,600	20,400
3. M_H/M_A	0.32	0.46	1.27
4. Wt. fr. of homopolymer, w	0.48 ^b	0.18	0.27
5. Wt. fr. of monomer A	0.62	0.37	0.80
6. Wt. fr. of H in (H + A), p	0.77	0.44	0.34
7. Vol. ratio of H to A, q	3.4	0.79	0.51
8. Vol. ratio q, theoretical ⁵	0.23	0.12	0.03

^aThe block having the same monomer as the homopolymer is designated A.

^bAt 90°C.

Table II
Polymer-Polymer Interaction Parameter Λ^a

	f_A^b	λ_o	λ_1	λ_T	$\lambda_T/(1-f_A)^2$	$\Lambda_{12}/(1-f_A)^{2c}$
Mixture with PS (M_w 2400)	0.27	3.1	-0.3	-0.0063	-0.012	3.2
Mixture with PBD (M_w 26000)	0.73	0.50	0	-0.0014	-0.019	3.0
Average of Previous Results ^d					-0.009 \pm 0.003 ^e	2.8 \pm 0.4 ^e

^aGiven in units of J/cm³.

^bWt. fraction of the block in the block copolymer having the same monomer as the homopolymer.

^cEvaluated for 200°C and $\phi_1 = 0.5$.

^dRef. 2.

^eStandard deviation.

LEGEND TO FIGURES

Figure 1. The scattered intensity (or the output of the photodiode detector in mV) obtained from the mixture containing 25% of polystyrene (M_w 2400) at various heating rates. Solid line $4^\circ\text{C}/\text{min}$, dotted line $2^\circ\text{C}/\text{min}$, and broken line $0.5^\circ\text{C}/\text{min}$.

Figure 2. Cloud points obtained with mixtures containing polystyrene (M_w 2400). In regions I and II the mixture is transparent, while in regions III and IV it is turbid. The turbidity increases sharply on crossing from region III to IV at the temperatures indicated by triangles.

Figure 3. Cloud points obtained with mixtures containing polystyrene (M_w 3500).

Figure 4. Cloud points obtained with mixtures containing polybutadiene (M_w 26000).

Figure 5. The scattered intensity, initially obtained as a function of temperature, is replotted as a function of the weight fraction of polystyrene (M_w 2400) in the mixture. The difference in the rate of change of the turbidity with composition between the data at two temperatures, 80° and 140°C , is illustrated.

Figure 6. The solubility of homopolymer in the block copolymer, expressed as the weight fraction p of the homopolymer in the microdomain in which it is solubilized, is plotted against M_H/M_A , where M_H is the molecular weight of the homopolymer and M_A is that of the block in the copolymer having the same type of monomers. See the text for the explanation of the curve drawn in broken line. Point C represents a critical

point which is closely analogous to the critical consolute point in the composition-temperature phase diagram of a binary liquid mixture.

Figure 7. The phase diagram of the mixture containing polystyrene (M_w 2400), drawn to agree with the observed cloud points (circles) and the block copolymer transition temperatures (squares, determined by small-angle X-ray scattering¹). The liquid phases L_1 and L_2 consist of the disordered block copolymer and the polystyrene. Mesophase M_1 consists of ordered microdomains of the block copolymer swollen with polystyrene. Mesophase M_2 contains micellar aggregates of the block copolymer suspended in the medium of the polystyrene. The two lines AB and AC are considered to coalesce into a single line representing the transition temperature between the ordered and disordered structure. The features on the lower right, drawn in broken lines, are more speculative than the rest.

Figure 8. The phase diagram of the mixture containing polybutadiene (M_w 26000). Note that, in order to be consistent with the observed cloud points, the order-disorder transition temperature of the block copolymer has to decrease with increasing amount of the homopolymer, in contrast to the case shown in Fig. 7.

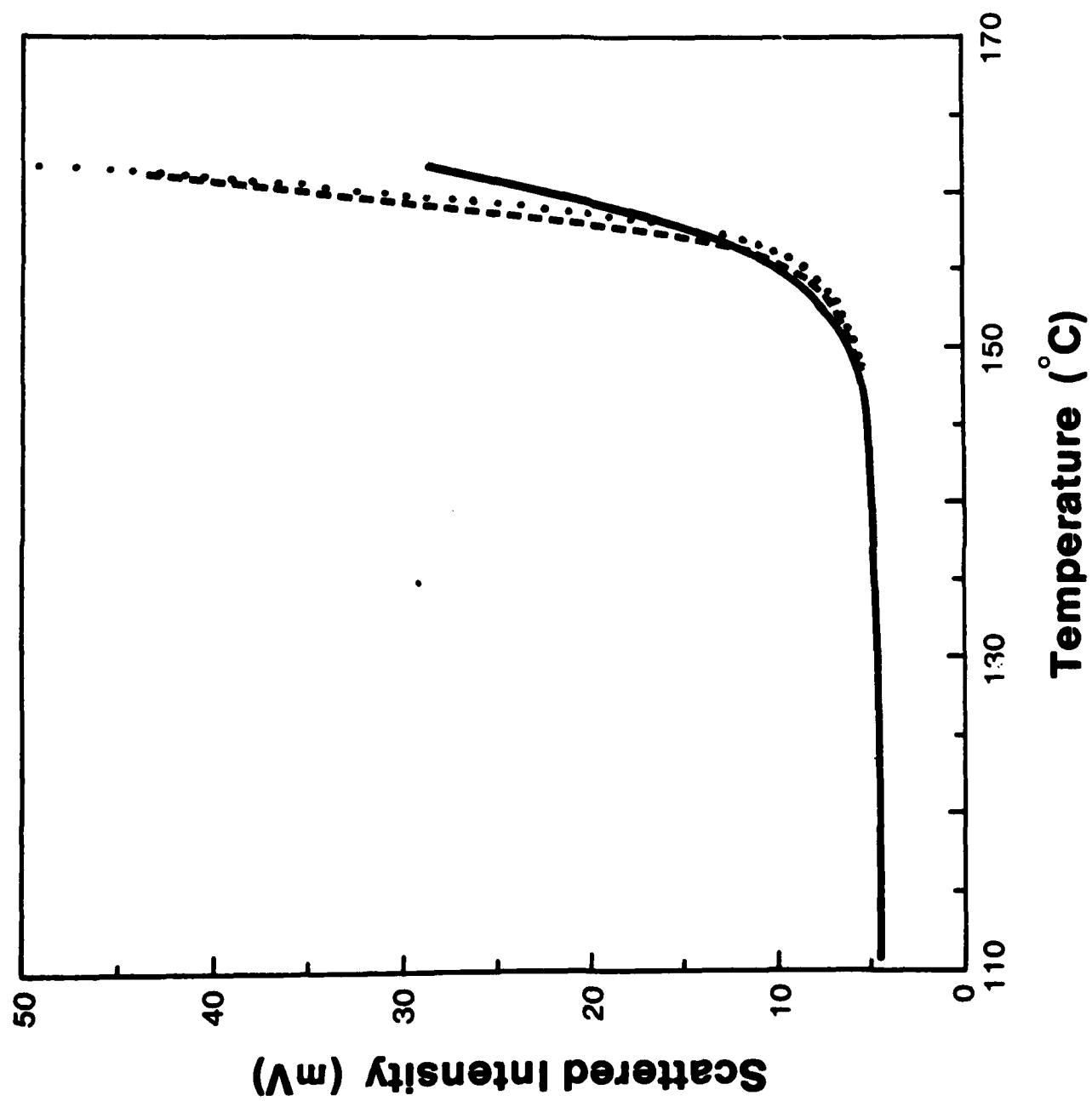


Figure 1

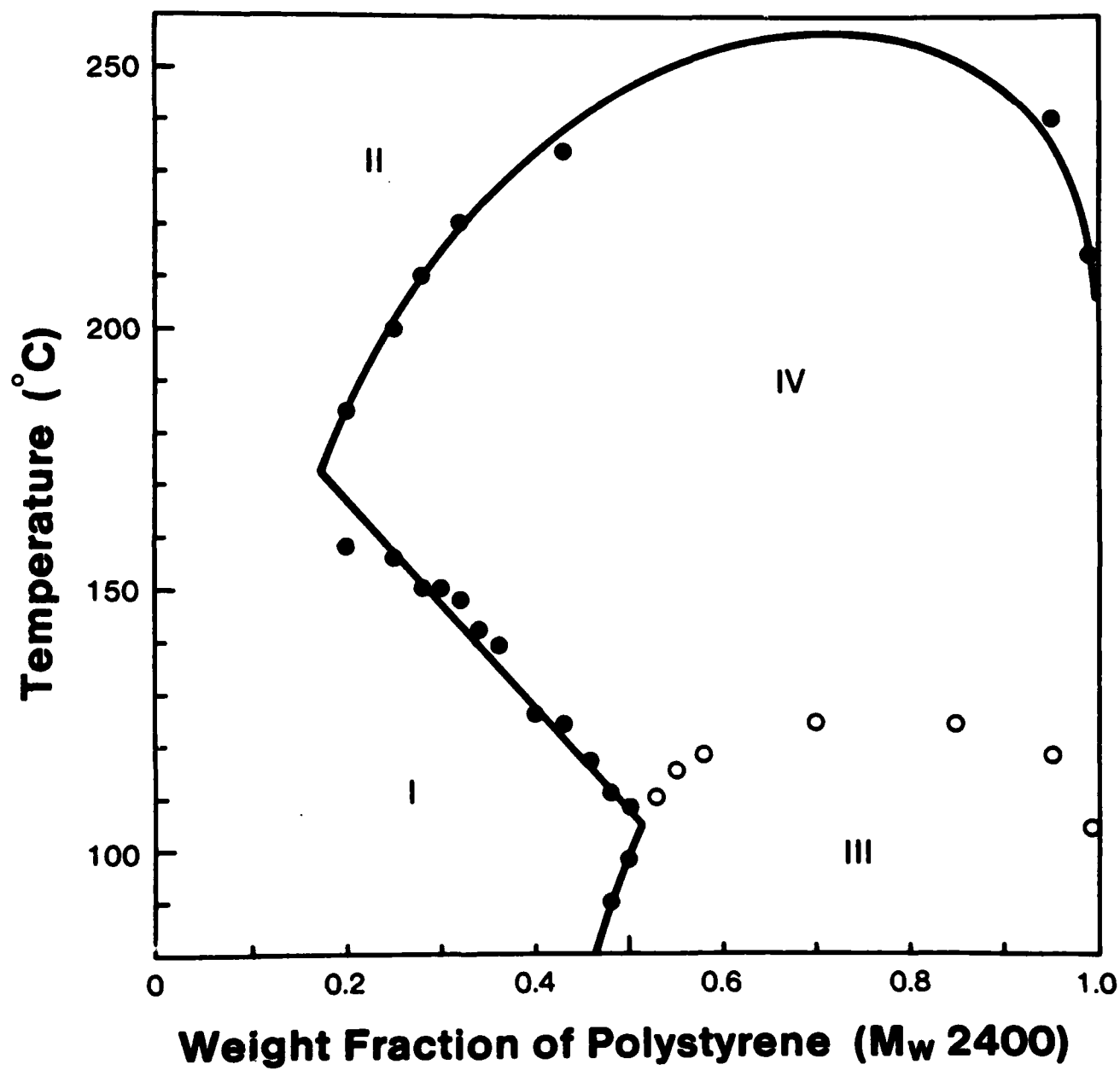


Figure 2

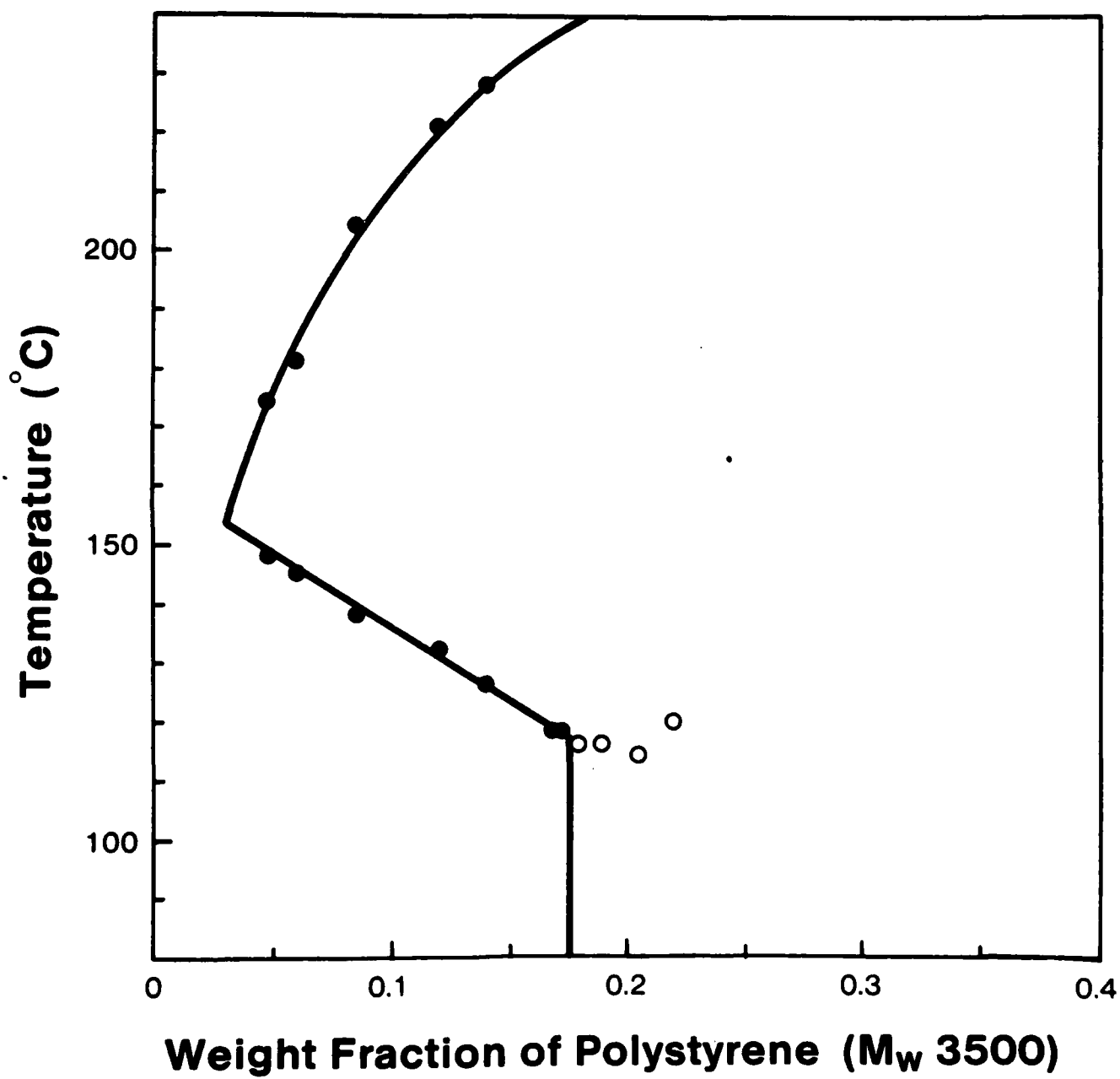


Figure 3

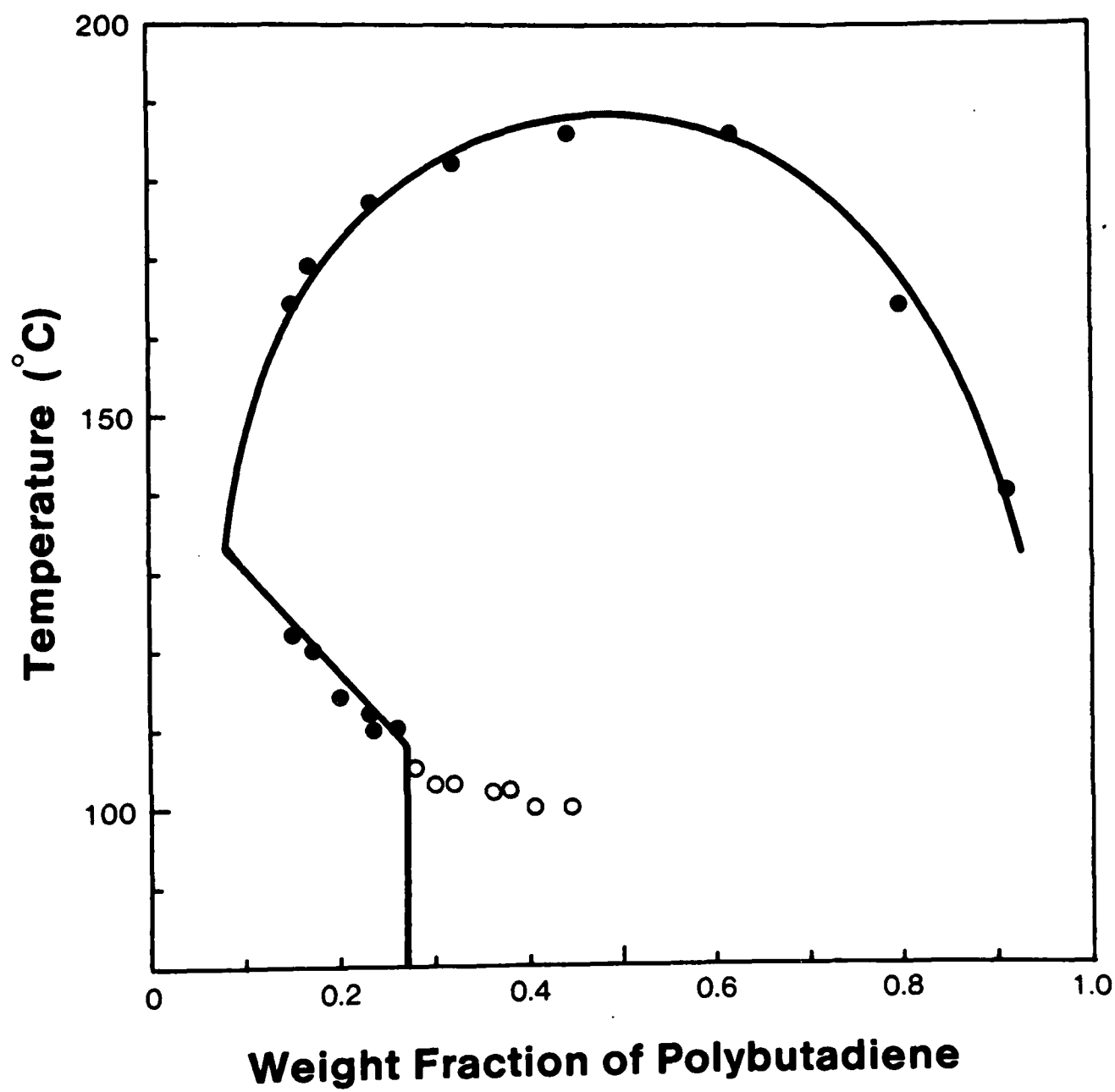
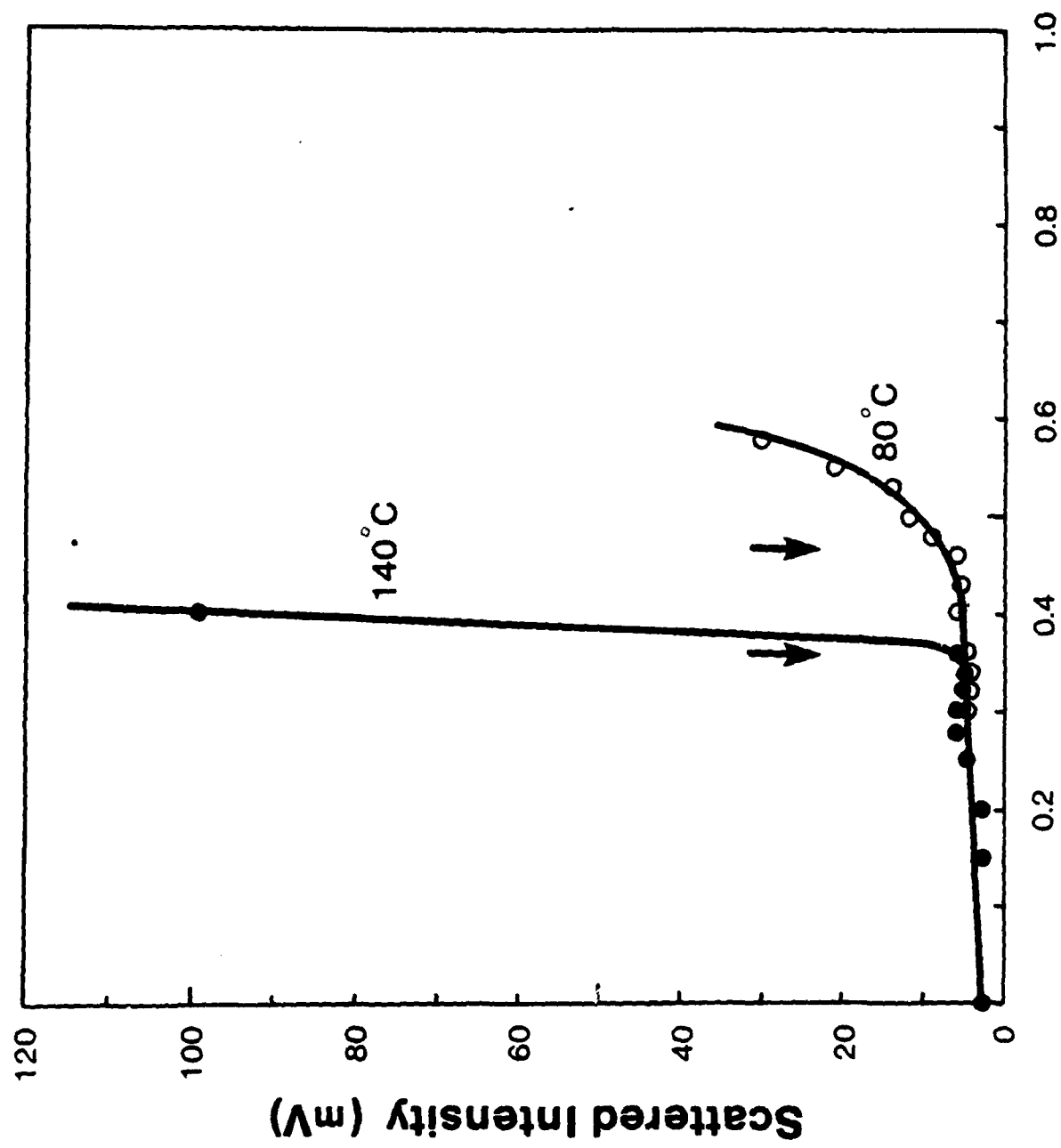


Figure 4



Weight Fraction of Polystyrene (M_w 2400)

Figure 5

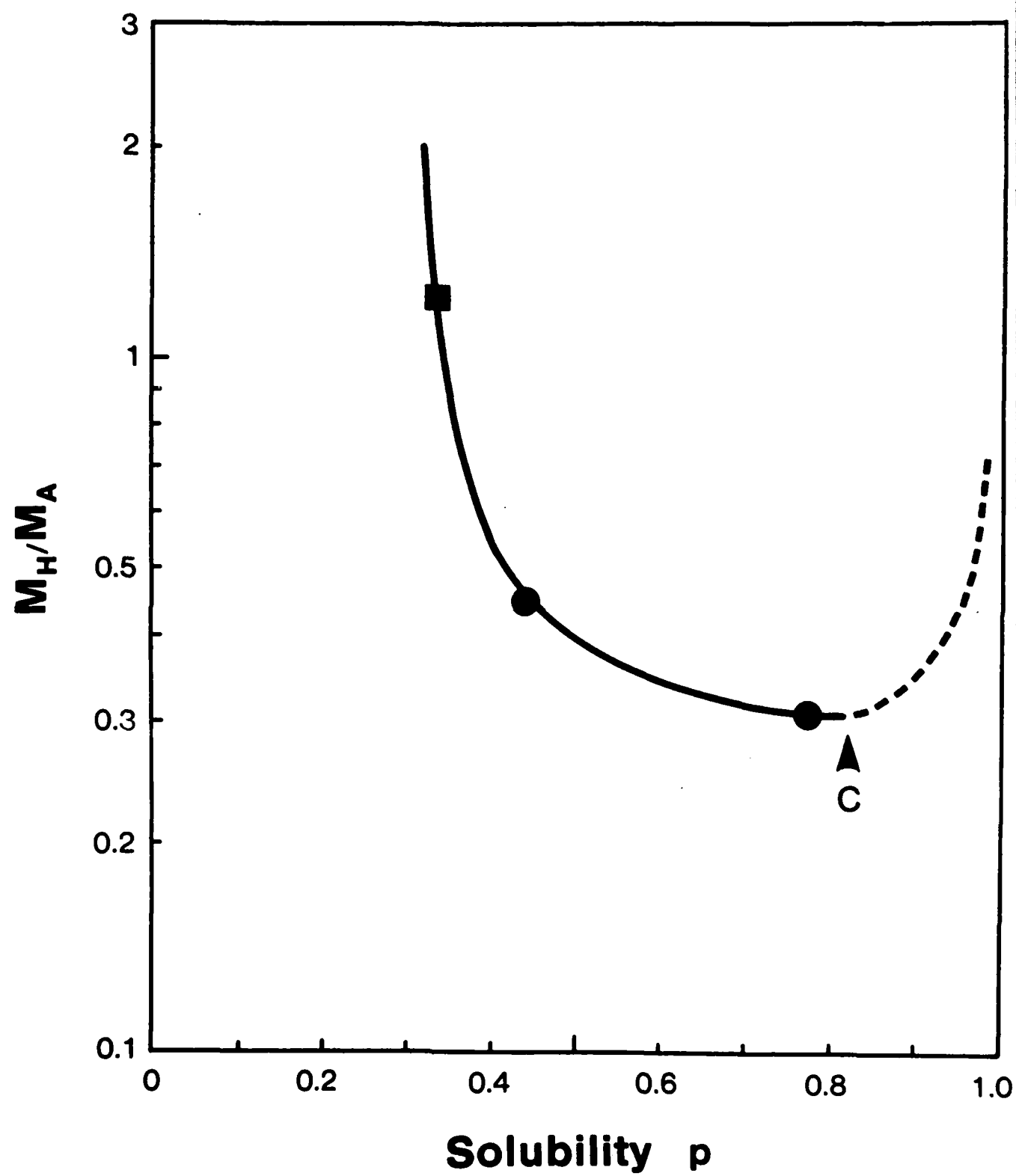


Figure 6

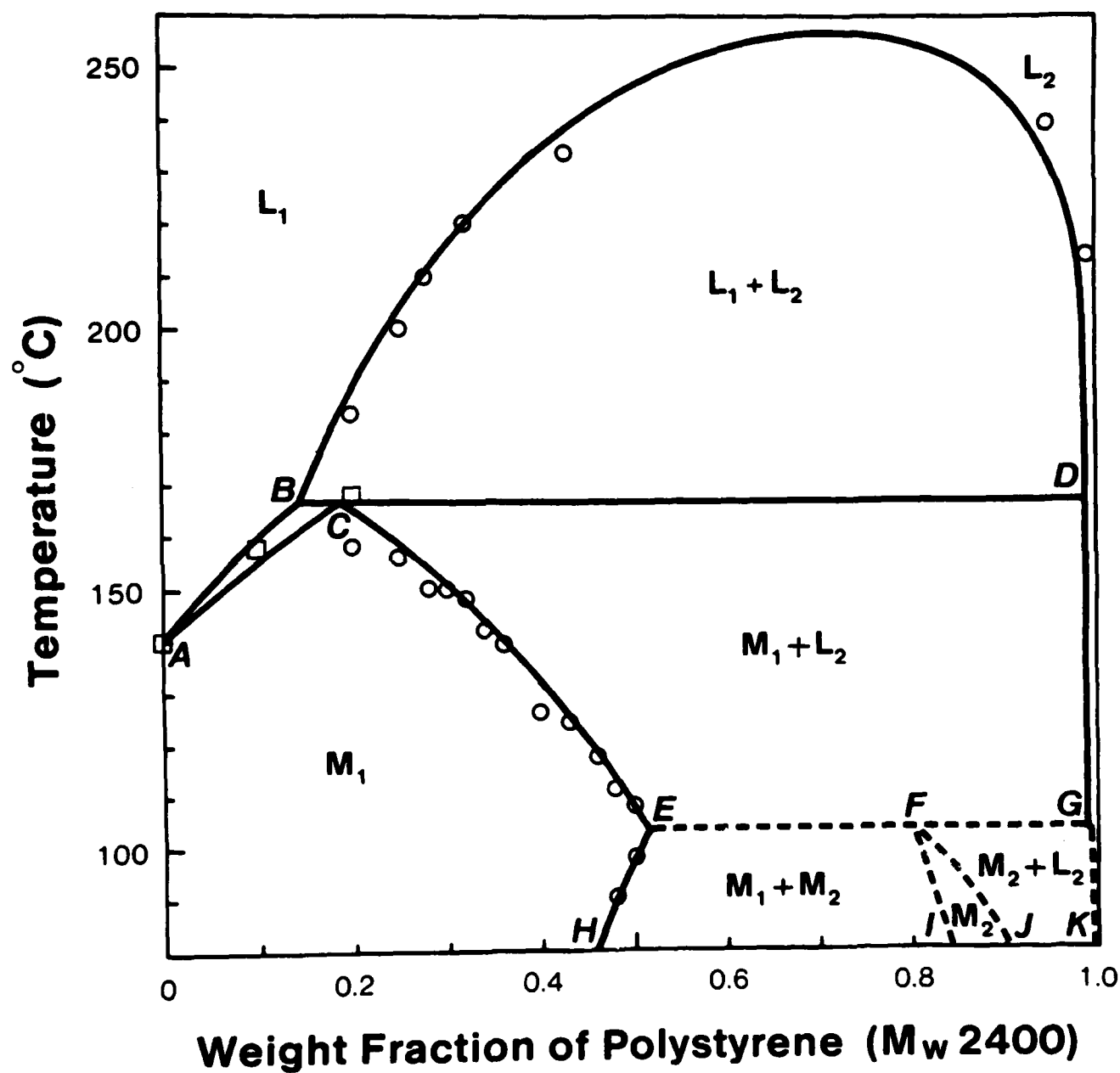


Figure 7

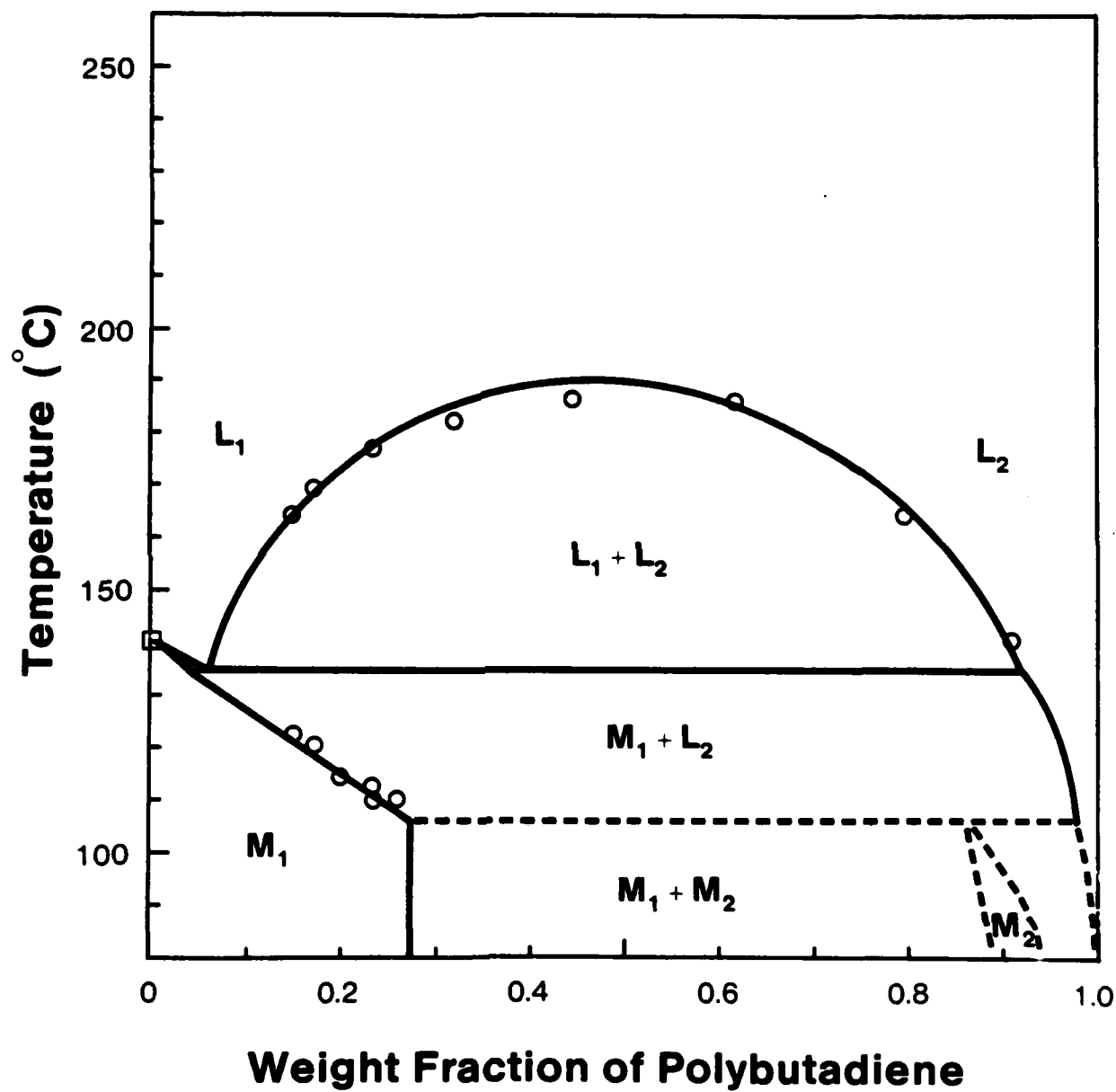


Figure 8

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